



Europäisches Patentamt  
European Patent Office  
Office européen des brevets

(11) Publication number:

**0 146 170**  
**A1**

(12)

## EUROPEAN PATENT APPLICATION

(21) Application number: **84201711.3**

(51) Int. Cl.<sup>4</sup>: **C 07 C 39/07, C 07 C 37/84**

(22) Date of filing: **26.11.84**

(30) Priority: **05.12.83 IT 2402583**

(71) Applicant: **ENICHIMICA S.p.A., Via Mozart 1,  
I-20122 Milan (IT)**

(43) Date of publication of application: **26.06.85**  
**Bulletin 85/26**

(72) Inventor: **Bialek, Jerzy, Wloscianska 2/52,  
PL-01-710 Warszawa (PL)**  
Inventor: **Plesnar, Marek, Hawajska 20/9,  
PL-00-776 Warszawa (PL)**  
Inventor: **Werle, Janina, Wilcza 62/7,  
PL-00-679 Warszawa (PL)**  
Inventor: **Bialy, Jan, Boduena 4/27, PL-00-011 Warszawa  
(PL)**

(84) Designated Contracting States: **AT BE CH DE FR GB LI  
LU NL SE**

(74) Representative: **Roggero, Sergio et al, Ing. Barzanò &  
Zanardo Milano S.p.A. Via Borgonuovo 10,  
I-20121 Milano (IT)**

(54) **Process for purifying 2,6 - xlenol.**

(57) Process for purifying raw 2,6-xlenol, comprising the following stages, carried out in succession:

- melting of raw 2,6-xlenol;
- slow and uniform cooling of said molten raw 2,6-xlenol until at least from 60% to 100% of its mass is separated as crystal solid;
- gradual heating of said crystal solid, after having separated the possibly remaining liquid fraction, up to a highest temperature value lower by 0,1-5 °C, then the solidification temperature of 2,6-xlenol, in order to causing surface melting on said crystals;
- separation of the thus obtained molten liquid phase and recovery of purified 2,6-xlenol.

**EP 0 146 170 A1**

Disclosure

The present invention relates to the purification of raw 2,6-xyleneol, by means of a melting/crystallizing process carried out in the absence of solvents or thinners.

5        2,6-Xyleneol is the starting material for the production of polyphenyleneoxide, a valuable polymer used in the art for several applications.

10        The limited availability of 2,6-xyleneol deriving from sources such as the heavy fractions from the distillation of coal, and the problems related to the separation from such sources of 2,6-xyleneol at a suitable purity, have promoted the development of processes for the chemical synthesis of 2,6-xyleneol. Presently, 2,6-xyleneol is produced nearly exclusively by the catalytic methylation of phenol with methanol. In this reaction, together with the desired product 2,6-xyleneol, also not negligible quantities are formed of cresols and xyleneol isomers of 2,6-xyleneol. In the reaction mixture also unconverted reactants, water and several byproducts are present. By separating such a reaction mixture by distillation and rectifying, it is possible to obtain a 2,6-xyleneol with a purity of about 95 - 98%.

25        However, in the production of polyphenylene oxide by the oxidative polymerization of 2,6-xyleneol, a very pure 2,6-xyleneol is required, in any case with a purity higher than 99%. Thus, 2,6-xyleneol obtained by chemical synthesis undergoes, according to the art known, purification processes, by means of crystallization, mainly from solvents. Selective solvents used to this purpose are e.g. aliphatic organic acids and water/ethylene glycol

30

ol mixtures.

However, the purification of raw 2,6-xyleneol on the basis of the crystallization from solvent is generally a complex and also expensive process, due to the need of recovering and regenerating the solvent used to this purpose.

In the disclosure of the French Pat. N° 1.583.244, a process is disclosed for the purification of raw 2,6-xyleneol, which consists essentially in heating said solid raw 2,6-xyleneol, slowly and gradually, so as to cause only a partial melting of it. In this way, a molten liquid fraction of raw 2,6-xyleneol is separated, which is richer of impurity than the fraction which did not undergo the melting.

Such an operating way, if on one side eliminates the drawbacks arising from the use of the solvents, on the other does not allow a purified 2,6-xyleneol to be obtained, at a purity level as high as desirable.

The present invention is based on the observation that a slow and uniform cooling of molten raw 2,6-xyleneol allows 2,6-xyleneol crystals to be obtained, which are richer of impurities in correspondence of the surface and of surface layers of the same crystals. This allows a easier and more complete withdrawal of the impurities by the melting on the surface of the so obtained crystals, and after all makes it possible to obtain 2,6-xyleneol with unusually high purity.

Accordingly, the instant invention relates to the purification of raw 2,6-xyleneol by means of a process comprising the following steps carried out in succession:

- a) melting of raw 2,6-xyleneol;

- b) slow and uniform cooling of said raw 2,6-xyleneol, at a rate of from 0,1 to 10°C/hour, until at least from 60 to 100% of the mass is separated as a crystallized solid;
- 5 c) gradual heating of said crystallized solid, after having separated the possibly remaining liquid molten fraction, in a time of from 1 to 12 hours, up to a highest temperature value lower by from 0,1 to 5°C than the solidification temperature of 2,6-xyleneol,
- 10 to cause the melting on the surface of said crystals;
- d) separation of the molten liquid fraction so obtained and recovery of solid 2,6-xyleneol.

Raw 2,6-xyleneol, which is submitted to the purification process according to the present invention, is the

15 technical product, outcoming from the processes of synthesis of it, from phenol and methanol, which shows a content of about 95 - 98% of 2,6-xyleneol, and which contains impurities such as o-cresol, p-cresol, 2,4-xyleneol and 2,5-xyleneol.

20 According to the present invention, such a raw 2,6-xyleneol is caused to melt, generally at a temperature of the order of from 43 to 45°C (step a of the process) and is then cooled at a slow and uniform cooling rate of from 0,1 to 10°C/hour, and preferably of from 1 to 2°C/

25 hour, until from 60 to 80%, and preferably 80% about of the mass is separated as crystallized solid (step b of the process). By operating as described, the conditions are created which favour the growth of the crystals, and under which mainly single crystals are obtained, with

30 their surfaces being enriched of impurities, the successful performance being in this way made possible of puri

fication treatments.

According to the process of the present invention, said crystals, after the separation of the liquid molten fraction in the case of partial solidification, are submitted to a gradual heating, in a time of from 1 to 12 hours, up to a maximum temperature value which is lower by 0,1 to 5°C than the solidification temperature of 2,6-xylenol, with consequent superficial melting of the crystals (step c of the process).

In this step of the process, the molten liquid fraction can be withdrawn either in a continuous way, or batchwise, as a single fraction, or as a plurality of fractions with different impurity contents, and said separated fractions can be recycled to the purification process, after possible preliminary treatments, e.g., a rectifying treatment.

In any case purified crystalline 2,6-xylenol remains as a residue, with a purity generally higher than 99%, and even as high as 99,9%, which is recovered (step d of the process).

The process according to the present invention can be carried out in equipment of the tube nest type, in which inside the tubes the treatments are carried out of solidification/melting of 2,6-xylenol, and externally to the tubes a fluid circulates with controlled temperature.

The following Experimental Examples are illustrative and non limitative of the invention.

Example 1

Raw 2,6-xylenol (content of 2,6 xylenol 95,0% by weight, of o-cresol 4,9% by weight, other impurities

0,1% by weight), is submitted to a purification treatment inside the tubes of a tube crystallizer, having the structure of a heat exchanger.

5 The crystallizer consists of a set of vertical tubes, of length of 6 metres and diameter of 67 mm, welded to the upper and lower end plates of the equipment.

10 The inlet valve for feeding in the raw 2,6-xylenol is positioned atop, and the drain (discharge) valve is positioned at the bottom of the equipment. The bottom valve is connected, through pipings, to collecting tanks of purified 2,6-xylenol and of the fractions of contaminated 2,6-xylenol.

15 The crystallizer is moreover provided with a lining, so that the products can be heated or cooled by means of a fluid means circulating within the space surrounding the tubes. To such purpose, the crystallizer is connected with a heat exchanger in which the temperature is controlled of water sent to the crystallizer through  
20 a circulation pump.

After that the crystallizer has been heated at about 43°C by means of the water circulating outside the tubes, raw 2,6-xylenol is introduced inside the tubes of the crystallizer. The cooling is then started, with a constant cooling rate of 2°C per hour, until the thermocouple positioned in the centre of the vertical axis of  
25 tube set shows a temperature of 30°C.

At this time, the discharge valve on the bottom of the crystallizer is opened, and the solidified mass inside  
30 the tubes is heated, by increasing the temperature of circulating water at a rate of 2°C/hour for four hours.

During this time period a liquid fraction is collected of contaminated 2,6-xylenol (fraction 1). The temperature of circulating water is then gradually increased up to 42°C and is held at this value for the next 4 hours.

5 During this time period, another liquid fraction is collected of contaminated 2,6-xylenol (fraction 2). The temperature of circulating water is finally raised at 55°C, so as to melt the residual solid inside the tubes and to discharge purified 2,6-xylenol (end product).

10 In Table 1 the results are shown of the Example described hereinabove.

Table 1

	<u>Fraction</u>	<u>Parts by weight</u>	<u>2,6-xylenol (% by weight)</u>	<u>o-cresol (% by weight)</u>	<u>Solidifi- cation temp. (°C)</u>
15	Raw material	100	95,0	4,9	41,4
	Fraction 1	31	87,8	12,2	35,9
	Fraction 2	9	95,5	4,5	41,7
	End product	60	99,1	0,9	44,5

Example 2

The process is carried out as described in Example 1, initially cooling the mass of liquid raw 2,6-xylenol (containing 97,8% by weight of 2,6-xylenol and 2,2% by weight of o-cresol), at the rate of 1°C/hour, until a  
25 temperature of 32°C is reached at the centre of the vertical axis of the tube nest.

The discharge valve is then open and the temperature of circulation water is gradually raised to 42,5°C, and is maintained at this value for the next 6 hours. During  
30 this time period, a liquid fraction is collected of contaminated 2,6-xylenol (fraction 1). Successively,

the temperature of circulation water is gradually increased up to 44,5°C, and is kept at this value for the next 6 hours. During this time period, another liquid fraction is collected of contaminated 2,6-xylenol (fraction 2).

The temperature of water is finally raised, so as to melt the solid residue inside the tubes, and to discharge the purified 2,6-xylenol (end product).

In Table 2 the results are shown of the Example described above.

Table 2

<u>Fraction</u>	<u>Parts by weight</u>	<u>2,6-xylen ol (% by weight)</u>	<u>o-cresol (% by weight)</u>	<u>Solidifi cation temp. (°C)</u>
15 Raw material	100	97,8	2,2	43,5
Fraction 1	28	94,8	5,2	41,8
Fraction 2	19	98,8	2,0	43,6
End product	53	99,5	0,4	45,1

Example 3

The process is carried out as described in Example 1, introducing inside the tubes of the crystallizer raw 2,6-xylenol (containing 98,3% by weight of 2,6-xylenol, 1,1% by weight of o-cresol, and 0,5% by weight of 2,4- and 2,5-xylenol).

When the temperature inside the crystallizer is stabilized at 45°C, the mass is gradually cooled at the rate of 1°C/hour, until the temperature of 40°C is reached, at the centre of the vertical axis of tube nest. At this time, the bottom valve is opened, and the fraction 1 is collected.

The temperature of circulation water is then grad-



ually increased up to 44,5°C, and is held at such value for the next 6 hours. At this time the bottom valve is opened once more, and the fraction 2 is collected. Finally, the temperature of water is raised, so as to melt

5 the solid residue inside the tubes and to discharge the end product purified 2,6-xylenol.

In Table 3 the results are reported of the Example described above.

Table 3

Fraction	Percent- age by weight	2,6-xyleneol (% by weight)	o-cresol (% by weight)	m- & p-cresol (% by weight)	2,4- & 2,5- xylenol (% by weight)	Solidifi- cation tem per. (°C)
Raw material	100	98,3	0,05	1,1	0,5	44,3
Fraction 1	17	95,0	0,1	3,7	1,1	41,1
Fraction 2	15	98,5	0,03	1,0	0,85	44,2
End product	68	99,9	==	0,1	==	45,3

C l a i m s

1. Process for the purification of raw 2,6-xyleneol, characterized in that:

- 5 a) raw 2,6-xyleneol is molten;  
b) said molten raw 2,6-xyleneol is cooled, in a slow and uniform way, at a rate of from 0,1 to 10°C/hour, until  
10 al least 60% to 100% of the mass is separated as a crystalline solid;  
c) said crystalline solid is gradually heated, after having separated the liquid molten fraction possibly remaining, in a time of from 1 to 12 hours, up to a  
15 maximum temperature value lower by 0,1 - 5°C than the solidification temperature of 2,6-xyleneol, so as to cause the melting on the surface of said crystals;  
d) the molten liquid fraction so obtained is separated  
and purified solid 2,6-xyleneol is recovered.

2. Process as claimed in claim 1, characterized in that the raw 2,6-xyleneol which is submitted to the purification has a content of 2,6-xyleneol of from about 95% to about 98%.

20 3. Process as claimed in claim 1, characterized in that in the step b the cooling is carried out at a cooling rate of from 1 to 2°C/hour.

4. Process as claimed in claim 1, characterized in that in the step b the cooling is carried out till to  
25 solidify about 80% of charged batch.

5. Process as claimed in claim 1, characterized in that the molten liquid fraction which is formed in step c is collected continuously.

30 6. Process as claimed in claim 1, characterized in that the liquid molten fraction which is formed in step

c is collected intermittently.

7. Process as claimed in claim 1, characterized in that it is carried out in a tube nest crystallizer, equipped with a heat exchange fluid externally to the
- 5 same tubes.



European Patent  
Office

# EUROPEAN SEARCH REPORT

0146170

Application number

EP 84 20 1711

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.4)
D, Y	FR-A-1 583 244 (CHEMOPETROL ZAVODY PRO ZPRACOVANI ROPY OBOROVE REDITELSTVI) * Abstract; page 2, lines 4-30 *	1-7	C 07 C 39/07 C 07 C 37/84
Y	GB-A-1 066 032 (SOCIETE POUR L'EXPLOITATION DES PROCEDES AB-DER-HALDEN) * Claims; page 4, table II *	1-7	
			TECHNICAL FIELDS SEARCHED (Int. Cl.4)
			C 07 C 37/00 C 07 C 39/00
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 18-03-1985	Examiner WRIGHT M.W.
<p><b>CATEGORY OF CITED DOCUMENTS</b></p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons &amp; : member of the same patent family, corresponding document</p>			